



Standard Test Method for Long-Term Ring-Bending Strain of “Fiberglass” (Glass-Fiber-Reinforced Thermosetting-Resin) Pipe¹

This standard is issued under the fixed designation D5365; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 This test method covers a procedure for determining the long-term ring-bending strain (S_b) of “fiberglass” pipe. Both glass-fiber-reinforced thermosetting-resin pipe (RTRP) and glass-fiber-reinforced polymer mortar pipe (RPMP) are “fiberglass” pipes.

1.2 The values stated in inch-pound units are to be regarded as the standard. The SI units given in parentheses are for information only.

1.3 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.* A specific warning statement is given in 9.5.

NOTE 1—There is no known ISO equivalent to this standard.

2. Referenced Documents

2.1 *ASTM Standards:*²

D883 Terminology Relating to Plastics

D1600 Terminology for Abbreviated Terms Relating to Plastics

D3567 Practice for Determining Dimensions of “Fiberglass” (Glass-Fiber-Reinforced Thermosetting Resin) Pipe and Fittings

3. Terminology

3.1 *Definitions:*

3.1.1 *General*—Definitions are in accordance with Terminology D883 and abbreviations are in accordance with Terminology D1600 unless otherwise indicated.

3.2 *Definitions of Terms Specific to This Standard:*

¹ This test method is under the jurisdiction of ASTM Committee D20 on Plastics and is the direct responsibility of Subcommittee D20.23 on Reinforced Plastic Piping Systems and Chemical Equipment.

Current edition approved April 1, 2012. Published May 2012. Originally approved in 1993. Last previous edition approved in 2006 as D5365 - 06. DOI: 10.1520/D5365-12.

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard’s Document Summary page on the ASTM website.

3.2.1 *end point*—the failure of the test specimen. The failure mode may be catastrophic, characterized by a sudden fracture through the pipe wall in the area of greatest strain.

3.2.2 *fiberglass pipe*—tubular product containing glass-fiber reinforcements embedded in or surrounded by curing thermosetting resin. The composite structure may contain aggregate, granular or platelet fillers, thixotropic agents, pigments, or dyes; thermoplastic or thermosetting liners or coatings may be included.

3.2.3 *reinforced polymer mortar pipe (RPMP)*—fiberglass pipe with aggregate.

3.2.4 *reinforced thermosetting resin pipe (RTRP)*—fiberglass pipe without aggregate.

4. Summary of Test Method

4.1 This test method consists of subjecting submerged-pipe ring specimens to various increasing deflections induced by a constant load and monitoring the time to failure. A minimum of 18 samples are required. Test temperatures are obtained by testing in a fluid environment where the temperature is controlled.

4.2 The long-term ring-bending strain is obtained by an extrapolation to 50 years of a log-log linear regression line for failure strain versus time.

NOTE 2—It is the consensus of Subcommittee D 20.23 that the log-log linear regression analysis of test data is a conservative approach and is representative of standard industry practice. However, a task group has been formed to evaluate alternative non-linear analysis methods.

5. Significance and Use

5.1 This test method determines the long-term ring-bending strain of pipe when deflected under constant load and immersed in a chemical environment. It has been found that effects of chemical environments can be accelerated by strain induced by deflection. This information is useful and necessary for the design and application of buried fiberglass pipe.

NOTE 3—Pipe of the same diameter but of different wall thicknesses will develop different strains with the same deflection. Also, pipes having the same wall thickness but different constructions making up the wall may develop different strains with the same deflection.

*A Summary of Changes section appears at the end of this standard

6. Apparatus

6.1 *Loading Device*—The testing apparatus shall be suitable for maintaining a constant load on the test specimen.

6.2 *Load Application*—The load may be applied to the test specimens using any of three alternative pairs of parallel loading surfaces; flat plates, rods or bars of a length at least as long as the pipe ring and of sufficient strength and stiffness to ensure a straight loading surface throughout the test. The same type of loading device shall be used for each specimen in a test series. In order to achieve uniform strain along the pipe, use 0.25-in. (6-mm) thick elastomeric pads between the parallel loading surfaces and the pipe ring (see [Note 2](#)).

6.2.1 *Flat Plates*—The plates shall have a minimum 6-in. (152-mm) width.

6.2.2 *Bars*—The bars shall have a flat contact surface of 0.75 ± 0.25 in. (19 ± 6 mm).

6.2.3 *Rods*—The rod diameter shall be 2 ± 0.25 in. (51 ± 6 mm) for pipe rings 12 in. (305 mm) and greater in diameter. For smaller pipes, the rod diameter shall be 1 ± 0.25 in. (25 ± 6 mm).

6.3 *Environment Containment*—A test enclosure of sufficient size to fully immerse the test specimens shall be used to contain the test solution. The enclosure shall not chemically affect the test solution.

NOTE 4—Elastomeric pads with a hardness of Shore A40 to 70 have been used successfully.

7. Test Specimens

7.1 The test specimens shall be ring sections taken from sample(s) of pipe selected at random from a normal production run. The test specimens shall have a minimum length of one nominal pipe diameter or 12 in. (305 mm) ± 5 %, whichever is less. Treat the cut edges of the specimens by the same procedure as production products.

8. Test Conditions

8.1 The standard temperature shall be $23 \pm 5^\circ\text{C}$ ($73.4 \pm 9^\circ\text{F}$).

9. Procedure

9.1 *Test Specimen Measurements:*

9.1.1 *Wall Thickness*—Determine in accordance with Test Method [D3567](#).

9.1.2 *Inside Diameter*—Determine in accordance with Test Method [D3567](#) at both ends prior to deflection and average the measurements.

NOTE 5—It is recommended that the inside diameter be measured with the axis vertical.

9.2 Place the test apparatus into the test enclosure.

9.3 Place the pipe ring in the test apparatus (see [Fig. 1](#)) and apply force to deflect the specimen at a rate not to exceed 10 % of its diameter per minute while keeping the top and bottom loading devices (plates, bars, or rods) of the apparatus as near parallel as practical. When the desired deflection is obtained cease adding load to the apparatus.

NOTE 6—Alignment of the specimen within the loading devices is

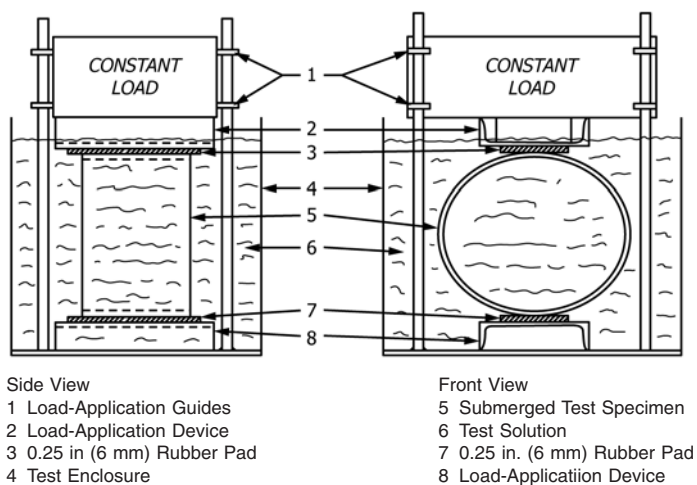


FIG. 1 Long-Term Ring Bending Test Apparatus

critical. The loading devices should not only be parallel with the load points 180° opposite, but the pipe ring should also be centered between the load-application guides. Additionally, the load-application guides should permit complete vertical freedom of movement, so the specimen remains under constant load.

9.4 Measure the vertical inside diameter of the deflected pipe specimen at both ends to the nearest 0.01 in. (0.25 mm). Average the measurements and determine the initial deflection by subtracting the average vertical inside diameter after loading from the measurement determined in [9.1.2](#).

NOTE 7—Deflections in excess of 28 % of diameter may cause local flattening of the pipe and lead to erratic test results. For deflections approaching 28 %, improved accuracy is obtained by use of strain gages or by establishing, for each pipe product, a calibration of deflection versus measured strain. This calibration technique may also be useful at all deflection levels.

9.5 Introduce the test solution to completely submerge the pipe ring. The solution may be added prior to loading the pipe ring and should be added within 30 min of loading the pipe ring. Testing time commences only after both specimen loading (deflection) and the addition of solution are complete. (**Warning**—Since the failure mode could be catastrophic, take precautions to prevent or contain splashing or spilling of the test solution or other damages resulting from the sudden collapse of the pipe specimen.)

9.6 Periodically check and maintain the test solution within ± 5 % of the specified strength or concentration for the duration of the test. The test specimen must remain completely submerged.

NOTE 8—As some solutions become more concentrated with the evaporation of water, care must be exercised in replenishment to prevent a build-up in strength. It may be necessary, with some reagents, to periodically clean the deflected specimen and replace the test solution with a fresh mixture. The use of plastic film, cut carefully to fit around the test apparatus and floated on the top of the test solution, has been found helpful in reducing evaporation.

9.7 Continuously monitor the decreasing pipe-ring inside vertical diameter versus time or inspect the loaded specimen at

least at the frequency given below and measure the pipe specimen inside vertical diameter:

Hours	Inspect at Least
0 to 20	Every hour
20 to 40	Every 2 h
40 to 60	Every 4 h
60 to 100	Every 8 h
100 to 600	Every 24 h
600 to 6000	Every 48 h
After 6000	Every week

Determine the deflection by subtracting the inside vertical diameter from the measurement determined in 9.1.2.

NOTE 9—Decreasing diameter of the pipe ring (deflection change) may be monitored with an appropriate indicator on the apparatus above the solution and submerged specimen.

9.8 Calculate the end point (failure time and failure deflection) in accordance with 10.1.

9.9 Record the following data:

- 9.9.1 Average pipe-wall thickness,
- 9.9.2 Average inside pipe diameter before deflection,
- 9.9.3 Average inside pipe diameter after deflection,
- 9.9.4 Initial deflection,
- 9.9.5 Type of loading device,
- 9.9.6 Type, location and time of any distress of the pipe wall,
- 9.9.7 Failure deflection and time at the end point, and
- 9.9.8 Type of failure.

9.10 To determine the regression line and the lower confidence level, a minimum of 18 samples is required. Distribution of data points shall be as follows:

Hours	Failure Points
10 to 1000	At least 4
1000 to 6000	At least 3
After 6000	At least 3
After 10 000	At least 1

9.10.1 Those specimens that have not failed after more than 10 000 h may be included as failures to establish the regression line. Use of these data points may result in a higher or lower extrapolated value.

NOTE 10—Non-failed specimens may be left under test and the regression line recalculated as failures are obtained.

10. Calculation

10.1 Determine the failure time and deflection:

10.1.1 The failure deflection and failure time shall be the last values noted prior to the fracture occurrence.

10.2 *Long-Term Ring-Bending Strain:*

10.2.1 Compute the failure strain for each failed specimen as given in 10.2.1.1 and 10.2.1.2.

10.2.1.1 Crown and invert failures:

$$\varepsilon_f = \frac{4.28(e)(\Delta_f)}{(D + \Delta_f/2)^2}$$

where:

ε_f = failure strain in inches per inch (millimetres per millimetre),

e = wall thickness in inches (millimetres) in accordance with 9.1.1 (see Note 11),

D = mean diameter in inches (millimetres) (ID in accordance with 9.1.2 plus e in accordance with 9.1.1 or OD minus e), and

Δ_f = failure deflection in accordance with 10.1.

10.2.1.2 Springline failures:

$$\varepsilon_f = \frac{2.44(e)(\Delta_f)}{(D + \Delta_f/2)^2}$$

NOTE 11—The S_b calculations assume that the neutral axis is at the pipe-wall midpoint. For pipe-wall constructions that produce an altered neutral-axis position, it may be necessary to evaluate results by substituting $2\bar{y}$ for e . (\bar{y} is the distance from the appropriate pipe surface to the neutral axis.) Neutral-axis position must be determined with strain-gage couples.

10.2.2 Use for each specimen in the series, the log of the failure strain and the log of the failure time in hours as described in A1.4.1. Calculate S_b , the strain at 50 years (438 000 h).

10.2.3 If $S_{xy} > 0$ (see Annex A1.4.2.2), consider the data unsuitable.

10.2.4 Calculate r in accordance with A1.4.3.1. If r is less than the applicable minimum value given in Table A1.1, consider the data unsuitable.

10.2.5 Prepare a graph on a log-log diagram showing time to failure versus failure strain, with time plotted on the horizontal (x) axis and strain on the vertical (y) axis.

11. Reconfirmation of the S_b Regression Line

11.1 When a piping product has an existing S_b regression line, any change in material, manufacturing process, construction or liner will necessitate a screening evaluation as described in 11.2, 11.3, 11.4, 11.5, and 11.6.

11.2 Obtain failure points for at least two sets of specimens. Each specimen set shall consist of three or more specimens tested at the same initial strain level, as follows:

Hours to Failure (Average of Set)	Failure Points
10 to 200	At least 3
More than 1000	At least 3
Total:	At least 6

Include as failures those specimens that have not failed after 3000 h, provided they exceed the regression line.

11.3 Calculate and plot the 95 % confidence limits and the 95 % prediction limits of the original regression line in accordance with A1.4.6.2 using only data obtained prior to the change.

NOTE 12—Prediction limits define the bounds for single observations, whereas confidence limits define the bounds for the regression line.

NOTE 13—For 95 % confidence limits, there is a 2.5 % probability that the mean value for the regression line may fall above the UCL and a 2.5 % probability that the mean value for the regression line may fall below the LCL. For 95 % prediction limits, there is a 2.5 % probability that individual data points may fall above the UPL and a 2.5 % probability that individual data points may fall below the LPL.

11.4 Consider any changes in material or manufacturing process minor and permissible if the results of 11.2 meet the following criteria:

11.4.1 The average failure point for each specimen set falls on or above the 95 % lower confidence limit of the original regression line.